

*Porous material Analysis Toolbox based on OpenFOAM*

## **2023 AIAA SciTech**

TP-18: Ablation Material Responses



*NASA Ames Research Center Entry Systems Modeling (ESM)*

# **3D ablation modeling of silicone-coated heatshield compared to MEDLI2 in-flight data**

Jeremie Meurisse<sup>1</sup>, Georgios Bellas Chatzigeorgis<sup>1</sup>, Dinesh Prabhu<sup>1</sup>,

Arnaud Borner<sup>1</sup>, John Thornton<sup>1</sup>, Brett Cruden<sup>1</sup>, Nagi Mansour<sup>1</sup>,

Joshua Monk<sup>2</sup> & Brody Bessire<sup>2</sup>

<sup>1</sup>Analytical Mechanics Associates, Inc. at NASA Ames Research Center <sup>2</sup>NASA Ames Research Center

01/26/2023

*This material is a work of the U.S. Government and is not subject to copyright protection in the United States.*

#### **Introduction of PICA-NuSil**



NuSil, a silicone-based overcoat, was sprayed onto the MSL and Mars 2020 heatshields including their in-depth temperature instruments (MISP) to mitigate the spread of phenolic dust from PICA. The behavior and material response of the PICA-NuSil (PICA-N) system consists an open problem in the literature [3,4].

In order to better understand the behavior of the NuSil coating, dedicated experimental campaigns have been conducted, with the first one taking place in NASA's Langley, HyMETS facility in March 2019 [1,2] and the second one in the AHF at NASA ARC in November 2020.





A novel Material Response (MR) model for PICA-N was implemented in PATO that accounts for the observed temperature discontinuity and change of recession rate [4].



*Porous material Analysis Toolbox based on OpenFOAM*

#### **PATO overview**

PATO [4] is a modular research and development platform designed to the to test in models for porous materials submitted to high-temperature



#### **Surface modeling of the charred NuSil as pure silica**

 $\lambda$   $\tau$ S

the observations of a glassy layer on the post-test coated samples [1,2]. The multiple correcting or the multiples implemented in PATO to model the pure silica surface [3,4].





constant in the cine of the character **2. Modified SiO<sub>2</sub>** wall enthalpy  $(\Delta h_w)$  to

$$
B_{\rm c}' = \frac{\sum_{l=1}^{N_{\rm el}^{S}} \left[ B_{\rm g}'(z_{l, \rm pg} - z_{l, \rm w}) + z_{l, \rm e} - z_{l, \rm w} \right]}{\sum_{l=1}^{N_{\rm el}^{S}} (z_{l, \rm w} - z_{l, \rm ca})}
$$

$$
\left[ -\underline{\mathbf{k}} \cdot \partial_x T \right] \cdot \mathbf{n} = C_{\rm H}'(h_{\rm e} - h_{\rm w}) + \dot{m}_{\rm ca}(h_{\rm ca} - h_{\rm w}) + \dot{m}_{\rm pg}(h_{\rm pg} - h_{\rm w}) + q_{\rm rad}
$$



### Ablation simulations in HyMETS using charred NuSil modeled as SiO<sub>2</sub>



Fig. 1 Temperature and shape change at 30 sec [3,4].

**BLAYER**:  $p_w = 5.6 kPa$  |  $C_H = 0.18 \frac{kg}{m^2s}$  |  $h_e = 9.7 \frac{MJ}{kg}$ **Recession**:  $r_{exp} = 1.93$   $mm \mid r_{pato} = 1.98$   $mm$ **Modified NuSil B' table**:  $\Delta B_c' = 0.0195$  |  $\Delta h_w = 3 \frac{MJ}{kg}$ 2500 Wall TC1 TC<sub>2</sub> 2000 TC<sub>3</sub> Temperature (K)  $-$  TC4 1500 - Experiments - PATO 1000 500 10 20 30 40  $\Omega$ Time (s)

Fig. 2 Evolution in time of the temperature [3,4].

#### **Surface modeling of the charred NuSil as silicon oxycarbide**

and entropy were optimized using a  $\Sigma$  12<br>multi-**3.e Optimized SiOC**n. The  $\frac{\epsilon}{\sigma}$ 10 multi-3. Optimized SiOCn. The simulated temperature results were compared to PICA-N arc jet test cases (HyMETS and AHF-346). Note: The SiOC phase change was not included. The optimization solution was not unique.



was performed to analyze post-test sample surfaces from the HyMETS test campaign. The heat capacity of the charred NuSil surface was measured as a f**4. SiOC based on exp.** 1800 K. The heat capacity values were then used to build the latest surface model of the charred NuSil based on



#### **Ablation simulations using charred NuSil modeled as optimized SiOC**



The properties of the NASA9 database  $(c_p$ , h and s) were used in the Mutation++ library [6] to compute the equilibrium of the mixture which directly impacts  $B_c'$  and  $h_w$ . The PATO ablation simulations using the optimized SiOC properties for the charred NuSil surface model were compared to HyMETS and AHF-346 data.





#### **Comparison between the surface charred NuSil models and MEDLI2**



The 1D simulated temperatures using the charred NuSil surface modeled as **pure silica** showed the best agreement with the flight data from the thermal plugs MTH of the MEDLI2 suite [7]. Hereafter, this surface model will be used in the different PICA-N ablation simulations.

#### **Aerothermal environments for the Mars 2020 heatshield**

**Rarefied regime:** *SPARTA [8]* **Continuum regime:** *DPLR [9]* **Radiation:** *NEQAIR [10]*



DSMC **SPARTA** code was used to compute the environment in the rarefied regime from 0 to 43 sec. **DPLR** code was used to compute non-equilibrium supersonic and hypersonic flows around the aeroshell from 43 to 130 sec. Radiative heating was computed over the entire heatshield using the **NEQAIR** program on each CFD points. The convective peak heating occurred at 80 sec followed by the radiative one at 90 sec.

#### **3D ablation simulations of the Mars 2020 heatshield**



The heatshield geometry was discretized with an unstructured grid (100k cells including 60 in-depth). 3D PATO material response of the Mars 2020 heatshield using the charred NuSil **surface modeled as pure** SiO<sub>2</sub>. The total coating thickness was estimated to be 200 μm. The surface recession results indicate that the heatshield was **still fully covered by a layer of charred NuSil** after the Martian atmospheric entry.

#### **PICA-NuSil model compared to MEDLI2 flight data**



#### **PICA-NuSil model compared to MEDLI2 flight data**



#### **Summary of the PICA-NuSil model**

#### **Conclusion**

- 4 charred NuSil surface models developed:
	- *1. Pure silica* **:** best match with MEDLI2 data.
	- **2.** *Modified SiO*<sub>2</sub>: match HyMETS exp.
	- *3. Optimized SiOC* **:** match HyMETS/AHF exp.
	- **4. SiOC based on exp. :** match optimized SiOC.
- 3D ablation simulations for Mars 2020:
	- o *SPARTA:* rarefied regime using DSMC [0-43] sec.
	- o *DPLR:* CFD in fully turbulent regime [43-130] sec.
	- o *NEQAIR:* Radiative heating at each CFD points.
	- o *PATO:* 3D material response (T & rec.) using the charred NuSil surface modeled as pure silica.
	- o Model indicates that the Mars 2020 heatshield was still fully covered by a NuSil layer after entry.
	- o Good agreement was found between the PICA-N model (pure  $SiO<sub>2</sub>$ ) and the MEDLI2/MTH plugs.

#### **Future work**

- Development of a new model that couples pyrolysis and char blowing gases between DPLR and PATO.
- 3D ablation simulations of the Mars 2020 heatshield using the PICA-N model that will include the coupling of blowing gases. Results will be compared to MEDLI2 flight data.
- Further studies are needed to have a better understanding of the transition from laminar to turbulent.

#### **References**

[1] Bessire, Brody K., et al. "Progress Towards Modeling The Mars Science Laboratory PICA-Nusil Heatshield." 16th International Planetary Probe Workshop, 2019.

[2] Bessire, Brody K., et al. "Analysis of the PICA-NuSil HyMETS Arc-Jet Campaign." 11th Ablation Workshop, 2019. [3] Meurisse, Jeremie B.E., et al. "Progress towards modeling the ablation response of NuSil-coated PICA." 11th Ablation Workshop, 2019.

[4] Meurisse, Jeremie BE, et al. "Equilibrium model for the ablation response of silicone-coated PICA." International Journal of Heat and Mass Transfer 201 (2023): 123523.

[5] Stabler, Christina, et al. "Thermal properties of SiOC glasses and glass ceramics at elevated temperatures." Materials 11.2, 2018.

[6] Scoggins, et al. "Mutation++: MUlticomponent Thermodynamic And Transport properties for IONized gases in C++." SoftwareX 12, 2020.

[7] Hwang, Helen, et al. "Mars 2020 entry, descent, and landing instrumentation (MEDLI2)." 46th AIAA Thermophysics Conference. 2016.

[8] Gallis, Michael A., et al. "Direct simulation Monte Carlo: The quest for speed." AIP Conference Proceedings. Vol. 1628. No. 1. American Institute of Physics, 2014.

[9] Wright, Michael J., Todd White, and Nancy Mangini. Data Parallel Line Relaxation (DPLR) Code User Manual: Acadia Version 4.01. 1. National Aeronautics and Space Administration, Ames Research Center, 2009.

[10] Park, Chul. "Nonequilibrium air radiation (Nequair) program: User's manual." Unknow (1985).

[11] Lachaud, Jean, et al. "A generic local thermal equilibrium model for porous reactive materials submitted to high temperatures." International Journal of Heat and Mass Transfer 108 (2017).